

Important Points in soil classification in Foundation Design

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Abstract: It is necessary for the foundation engineer to classify the site soils for use as a foundation for several reasons: 1. To be able to use the data base of others in predicting foundation performance. 2. To build the geotechnical engineer's data base in the "art" application of design. 3. To maintain a permanent record which can be understood by others should problems later develop and outside parties be required to investigate the original design. Normally the Unified Soil Classification system (Table 2-1) with slight modifications is used in foundation design work. For example, in much foundation work it is academic whether a sand is well or poorly graded, but its density and the presence of gravel are of considerable interest. Whether a fine-grained cohesive soil is actually a clayey silt rather than a silty clay is not as important as identifying its strength and settlement characteristics

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1- Introduction

In foundation work the following terms are commonly used for cohesionless soil deposits:

Loose

Medium

Dense

Table 3-2 gives additional subdivisions with quantifications based on using field exploration data. Noting that these terms are both subjective and comparative[1], one should avoid using an excessive number of subdivisions. Similar subjective terms used for cohesive soils are:

Very soft

Soft

Medium

Stiff

Hard

Table 3-2 gives additional subdivisions with quantifications based on using field exploration data. Noting that these terms are both subjective and comparative, one should avoid using an excessive number of subdivisions. Similar subjective terms used for cohesive soils are: Very soft Soft Medium Stiff Hard Table 3-3 gives additional subdivisions but, again, with the subjective nature of these classifications a large number of subdivisions should be avoided. The foundation engineer relies primarily on a written description of the soil for assistance. Where a soil may simply classify as a SM or CH in the Unified soil system of Table 2-1, the geotechnical engineer would say "Reddish-brown, dense, silty sand, low plasticity, SM" or "Gray-blue stiff clay with trace

of sand, high plasticity, CH." The coloring and other distinguishing features such as "dense," "stiff," and "trace of sand" are self-explanatory, but note the ease of cross referencing these data to the next job the engineer might have in this area where the same type of material is encountered. The terms SM and CH would not convey much information alone, and it is altogether possible that another SM or CH could exist in the same boring at a different depth with very different foundation design properties (i.e., loose, gravelly, very dense, less silty, soft or hard, etc.). Other terms given in the next section may be used in the identification and classification of the soil at a site for foundation suitability and in preparing a report to the client on general findings and recommendations.

2- Soil Classification Terms

Identifying names, some of which are local in nature, are assigned to certain sizes or types of rock or soil formations, of which some of the principal ones are as follows:

1. Bedrock. Rock in its native location, usually extending greatly both horizontally and vertically. This material is generally overlain by soil of varying depths. If exposed, the outer portions may become weathered. Bedrock varies from igneous rocks, generally the hardest and formed from molten magma, to metamorphic rocks formed from metamorphosing sedimentary rocks under great heat and pressure, to sedimentary rocks formed as a combination of chemical action and pressure from overlying soil deposits. Rocks may be solid, but the interface with the overlying soil

may be much fractured and eroded and may contain voids from several weathering processes. Depending on the geologic history of the area, the rocks may be much fractured, folded, and faulted. Various textbooks on geology should be consulted for further information, especially concerning particular areas [e.g., Legget (1962), Thornbury (1965), both with extensive references].

2. Boulders. Smaller pieces of material which have broken away from the bedrock, usually 250 to 300 mm or more in dimension (Table 2-2). Pieces smaller than boulders may be called cobbles (50 to

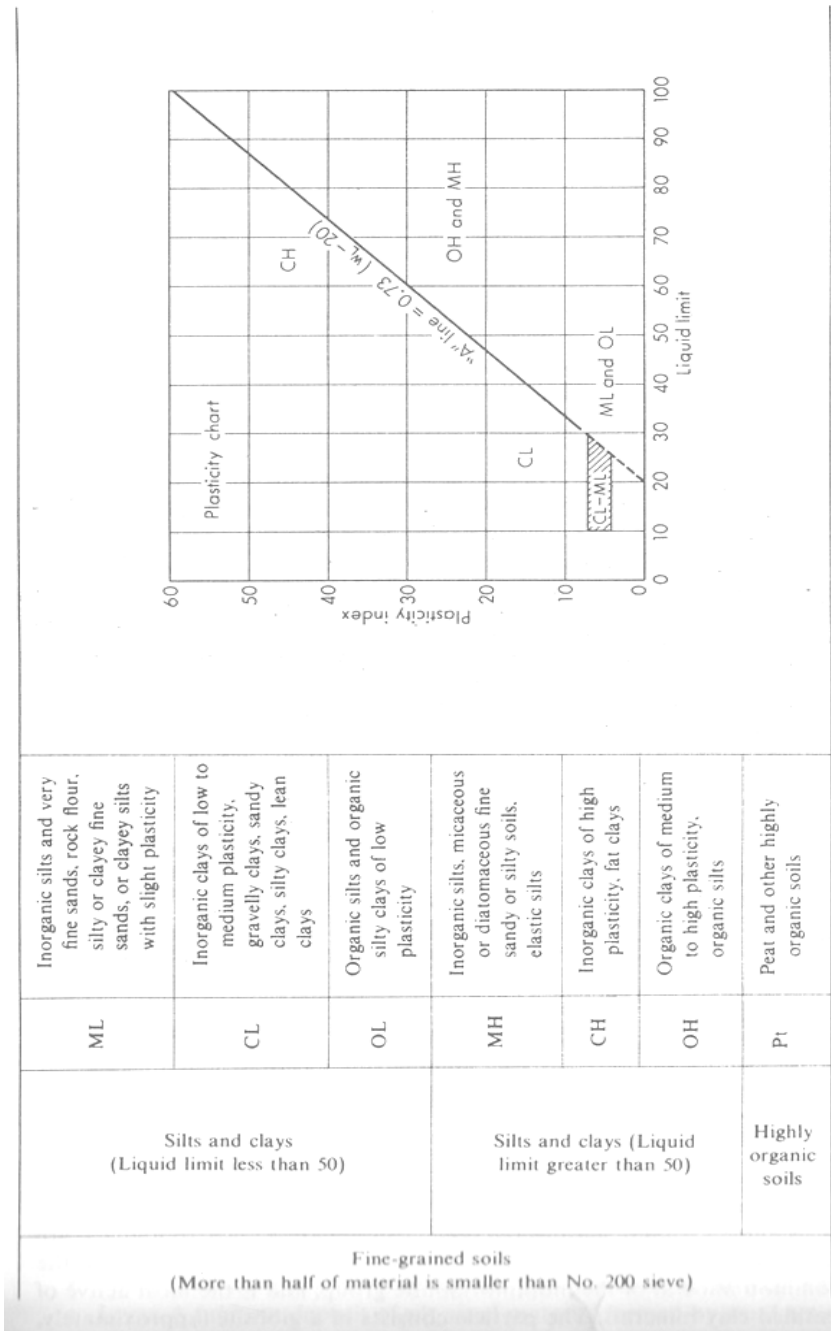
75 mm minimum size) or pebbles (3 to 5 mm minimum size).

3. Gravel. Common term used to describe pieces of rock from about 150 mm maximum to less than 5 mm dimensions. May be crushed stone when manufactured, bank-run gravel when excavated from a naturally occurring deposit and containing finer material, or pea gravel if it has been screened to sizes 5 to 3 mm (pea size). Gravel is a cohesionless material; that is, it does not possess particle adhesion or attraction.

Laboratory classification criteria		Typical names		Group symbols		Major divisions	
$C_u = \frac{D_{60}}{D_{10}}$ greater than 4; $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3 Not meeting all gradation requirements for GW		Well-graded gravels, gravel-sand mixtures, little or no fines		GW		Clean gravels (Little or no fines)	
		Poorly graded gravels, gravel-sand mixtures, little or no fines		GP		Gravels with fines (Appreciable amount of fines)	
Above "A" line with I_p between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits below "A" line or I_p less than 4 Atterberg limits above "A" line with I_p greater than 7		Silty gravels, gravel-sand-silt mixtures		GM*		Gravels (More than half of coarse fraction is larger than No. 4 sieve size)	
		Clayey gravels, gravel-sand-clay mixtures		GC		Sands (More than half of coarse fraction is smaller than No. 4 sieve size)	
$C_u = \frac{D_{60}}{D_{10}}$ greater than 6; $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ between 1 and 3 Not meeting all gradation requirements for SW		Well-graded sands, gravelly sands, little or no fines		SW		Clean sands (Little or no fines)	
		Poorly graded sands, gravelly sands, little or no fines		SP		Sands with fines (Appreciable amount of fines)	
Limits plotting in hatched zone with I_p between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits below "A" line or I_p less than 4 Atterberg limits above "A" line with I_p greater than 7		Silty sands, sand-silt mixtures		SM*		Coarse-grained soils (More than half of material is larger than No. 200 sieve size)	
		Clayey sands, sand-clay mixtures		SC			

Determine percentages of sand and gravel from grain-size curve. Depending on percentage of fines (fraction smaller than No. 200 sieve size), coarse-grained soils are classified as follows:
 Less than 5 percent GW, GP, SW, SP
 More than 12 percent GM, GC, SM, SC
 5 to 12 percent *Borderline* cases requiring dual symbols†

Table 1



Material	Upper, mm	Lower, mm	Comments
Boulders (or cobbles)	300 +	75	
Gravel	75	2-5	No. 4 or No. 10 sieve
Sand	2-5	0.074-0.05	No. 200 sieve or less
Silt	0.074-0.05	0.006	
Rock flour	0.006		Inert
Clay	0.002	0.001	Partic attraction
Colloids	0.001		

Table 2

4. Sand. Mineral particles smaller than gravel but larger than about 0.05 to 0.074 mm. May be fine, medium, or coarse, depending on the size of the majority of the particles. Sand is a cohesionless material; however, if it is damp or moist, the surface tension of the water may give an apparent cohesion which disappears when the material dries or becomes saturated. Sand is a favorable construction material. It has excellent bearing capacity if confined. Unconfined medium to fine sand will flow from beneath foundations, pavements, etc., and this process can be accelerated by water flowing through and by wave or stream action eroding it. Since water flows easily through sand, any retaining structure for water must contain non sand materials such as silts, clays, or mixtures of both. Excavations in sand will stand on slopes of about 16' to 1:1 or less. Excavations steeper than this are potentially unstable.

5. Silt. Mineral particles ranging in size from 0.05 to 0.074 mm maximum to 0.002 to 0.006 mm. It is called organic silt if it contains appreciable quantities of organic materials, and inorganic silt if no organic materials are present. Silt usually exhibits some cohesion, or particle attraction and adhesion, and may also have apparent cohesion, which is lost upon drying. Generally the cohesion in silt soils is due to the presence of clay particles dispersed through the mass. Often as little as 5 to 8 percent clay particles will give significant clay characteristics to a silt. Silt is generally not a very good foundation material unless dry or highly compressed into a sedimentary rock (siltstone). It is normally loose and quite compressible. As a construction material, it is difficult to compact unless the water content is carefully controlled. Material too wet is likely to weave (sometimes termed bull's liver) ahead of compaction equipment.

6. Clay. Mineral particles smaller than silt size (most authorities currently take clay particles as sizes 0.002 mm or smaller). If the particles are smaller than about 0.001 mm (1 μm), they may be called colloids. The clay particles are complex hydroaluminum silicates ($\text{Al}_2\text{O}_3 - n\text{SiO}_2 - k\text{H}_2\text{O}$, where n and k are numerical values of molecules

attached). Montmorillonite is a term for the most common mineral of the montmorillonite group, and is the most active of the identified clay minerals.

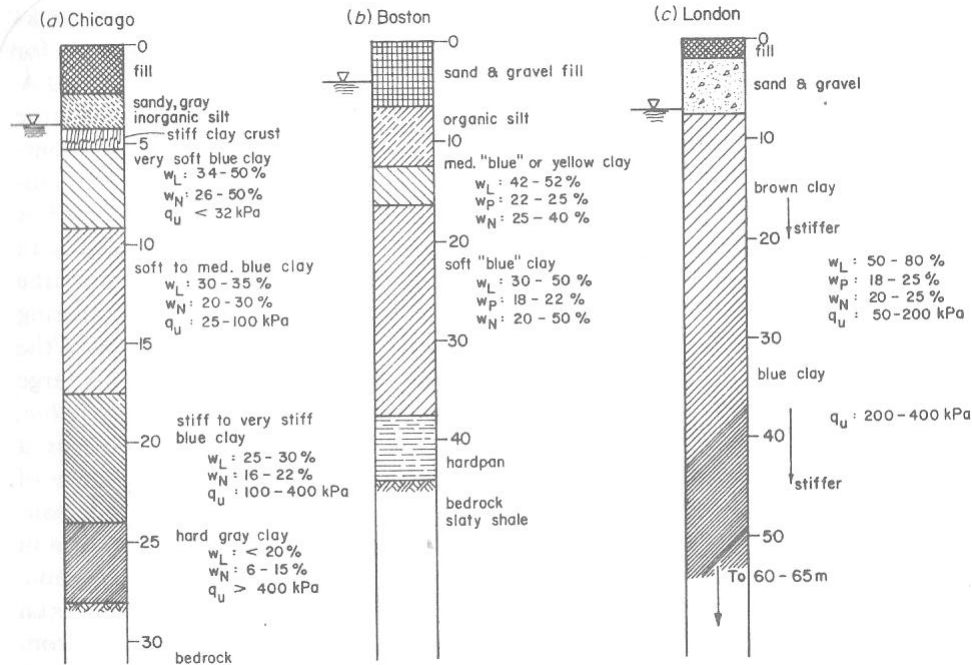
3- Review of experiments

The particle consists of a gibbsite (approximately, $\text{Al}_2\text{O}_3 - 3\text{H}_2\text{O}$) mass sandwiched between two silica sheets for a total thickness of

approximately 10 Å (angstroms). This material has a strong affinity for water, and may take on as much

as 200 Å of water for a total of 400 Å between clay particles. It is this affinity for water which accounts in a large part for the high shrinkage and swelling characteristics (activity) of the montmorillonite clays. The usual thickness of water is

probably 10 to 100 Å. Another clay mineral, illite, the most commonly occurring of the illite group, is less active than montmorillonite, since the adjacent silica layers are bonded with potassium ions, which provide a stronger bond than the water bond of the montmorillonite mineral. A third clay mineral, the most commonly occurring of the kaolin group, is kaolinite ($\text{Al}_2\text{O}_3 - 2\text{SiO}_2 - 2\text{H}_2\text{O}$), the least active of the clay minerals. Some other clay minerals are bentonite, which contains large quantities of montmorillonite and is highly active, halloysite, pyrophyllite, chlorite, and vermiculite. Clay is also defined as a cohesive material, that is, a material in which the particles tend to stick together from a combination of interparticle attractions and water effects. Kaolinite, illite, and montmorillonite are the most commonly occurring clay minerals[2]. Clays tend to be named in certain locales. For example, London clay is a clay found in London, England, with certain characteristics, Boston blue clay from Boston, Mass., has been reported by Casagrande and Fadum (1944) and others. Chicago blue clay from Chicago, Ill., has been extensively studied by Peck [see Peck and Reed (1954)] and others. Leda clay found in large areas of Ottawa Province in Canada has been extensively studied and reported [Crawford (1961), Soderman and Quigley (1965)].



Typical rofiles of the Boston, Chicago, and London, clay are illustrated in Fig. 2-4

Conclusion

- 1- Never use the soil that you do not know what activity it will have under structure pressure
- 2- Using of Rock in foundation of heavy structure can make the foundation site smart.

References

- 1- Begemann, H. (1974), "General Report: Central and Western Europe," European Symposium on Penetration Testing, Stockholm, Sweden, vol. 2.1, pp. 29-39.
- 2- Bell, A. L. (1915), The Lateral Pressure and Resistance of Clay, and the Supporting Power of Clay Foundations, in "A Century of Soil Mechanics," ICE, London, pp. 93-134.

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