

Generalized Projective Synchronization for Four Scroll attractor

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Abstract: This paper investigates an active control method is proposed to generalize projective synchronize two identical chaotic dynamical systems by constructing the response system no matter whether they are identical. The proposed technique is applied to achieve generalized projective synchronization for the Four - scroll attractor, where all state variables are in a proportional way. A strategy for practical implementation of a secure communication strategy is also discussed. Finally computer simulations are done to verify the proposed methods, and the results show that the obtained theoretic results are feasible and efficient.

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1. Introduction

Researchers from different areas, such as mathematicians, physicists, chemist, as well as control engineers have devoted themselves to examine the issue of synchronization over the past decade (Pacora and Carroll, 1990; Carroll and Pacora, 1991; Kocarev et al.,1992). Chaotic systems, in particular, have been applied to the development of secure communications, chemical reactions, biological systems and so on (Kocarev et al.,1992; Yuan and Jun, 2009; Zhu, 2009; Lu et al., 2002; Hua et al., 2005; Juan et al., 2012; Rafael and Yu, 2008). The system which received the most attention among chaotic communication systems perhaps is the Chua oscillator (Kocarev et al.,1992). This system belongs to general class of Lure systems (Khalil, 1996).

Chaos control and synchronization have attracted a great deal of attention from various fields since Huber published the first paper on chaos control in 1989 (Hubler, 1989). Over the last decades, many methods and techniques have been developed, such as OGY method (Ott et al., 1990), PC method (Pacora and Carroll, 1990; Carroll and Pacora, 1991), feedback approach, nonfeedback control methods, adaptive method, nonlinear control, active control, and backstepping design technique, etc (Wang et al., 2001, Elabbasy et al., 2004; Wang and Ge, 2001; Jiang et al., 2002; Sun and Zhang 2004).

There are many applications to chaotic communication (Fallahi and Leung, 2010; Elabbasy and El-Dessoky, 2010) and chaotic network synchronization (Chow et al., 2001). The techniques of chaotic communication can be divided into three

categories, (i) chaos masking (Kocarev et al., 1992), the information signal is added directly to the transmitter; (iii) chaos modulation (Boutayeb et al., 2002), it is based on the drive – response (master-slave) synchronization, where the information signal is injected into the transmitter as a nonlinear filter; (ii) chaos shift keying (Parlitz et al., 1992), the information signal is supposed to be binary, and it is mapped into the transmitter and the receiver. In these three cases, the information signal can be recovered by a receiver if the transmitter and the receiver are synchronized.

In 1963, Lorenz found the first classical chaotic attractor. In 1999, Chen found another similar but not topological equivalent chaotic attractor the Chen attractor (Chen and Ueta, 1999). In 2002, Lü and Chen found a new critical chaotic system (Lü and Chen, 2002), bearing the name of Lü system. It is noticed that these systems can be classified into three different types by the definition of Vaněšek and Čelikovsky (Vaněšek and Čelikovsky, 1996): the Lorenz system (Lorenz, 1963) satisfies the condition $a_{12} a_{21} > 0$, the Chen system (Chen and Ueta, 1999) satisfies $a_{12} a_{21} < 0$ and the Lü system (Lü and Chen, 2002) satisfies $a_{12} a_{21} = 0$, where a_{12} and a_{21} are the corresponding elements in the linear part matrix $A = [a_{ij}]_{3 \times 3}$ of the dynamical system.

The early projective synchronization (PS) is usually observable only in a class of systems with partial-linearity (Xu et al., 2001; Xu and Chee, 2002; Xu and Li, 2002, Wen and Xu 2005), but recently some researchers (Zhigang and Daolin,

2001; El-Dessoky, 2010) have achieved control of the projective synchronization in a general class of chaotic systems including non-partially-linear systems, and termed this projective synchronization as generalized projective synchronization (GPS) (Yan and Li, 2005; Changpin and Jianping, 2006; El-Dessoky and Salah, 2011).

In this paper, we generalize active control to GPS, and demonstrate this technique by some typical chaotic systems, for example, the chaotic Lorenz system and the chaotic Chen system such that GPS is achieved. The results from numerical simulations show that the method works well.

The paper is organized as follows. In Section 2, the generalized projective synchronization with active control is applied to synchronize two identical Four-scroll attractor and numerical simulations are presented to show the effectiveness of the proposed method. In Section 3, a scheme of secure communication based on the active control of Four-scroll chaotic system is presented. Conclusions are finally given in Section 4.

2. Generalized projective synchronization (GPS) of two identical Four-scroll chaotic attractor

The projective synchronization means that the drive and response vectors synchronize up to a scaling factor α , that is, the vectors become proportional. First, we define the GPS below. Consider the following chaotic system:

$$\dot{x} = f(x, t) \tag{1}$$

$$\dot{y} = g(y, t) + u(x, y, t) \tag{2}$$

where $x, y \in R^n$ are the state vector of the systems (1) and (2), respectively ; $f, g \in R^n \times R \rightarrow R^n$ are two continuous nonlinear vector functions, $u(x, y, t)$ is the vector control input. If there exists a constant α ($\alpha \neq 0$), such that $\lim_{t \rightarrow \infty} |y - \alpha x| = 0$, then the GPS of the systems (1) and (2) is achieved, and we call α is a scaling factor.

Now, we apply the adaptive feedback control method for generalized projective synchronization of two identical Four-scroll attractor (Lü et al., 2002 & 2004; Liu and Chen 2004; Elabbasy et al., 2006; El-Dessoky, 2010) which can be described by:

$$\begin{aligned} \dot{x} &= ax - yz \\ \dot{y} &= -by + xz \\ \dot{z} &= -cz + xy \end{aligned} \tag{3}$$

where a, b and c are positive control parameters. This system exhibits a strange attractor at the parameter values $a=0.4, b=12$ and $c=5$. This system bridges the gap between the Lorenz (Lorenz, 1963) and Chen attractors (Chen and Ueta, 1999), i.e. $a_{12} a_{21} = 0$. The divergence of the flow (3) is given by

$$\nabla \cdot F = \frac{\partial F_1}{\partial x} + \frac{\partial F_2}{\partial y} + \frac{\partial F_3}{\partial z} = a - b - c < 0,$$

Where

$$\begin{aligned} F &= (F_1, F_2, F_3) \\ &= (ax - yz, -by + xz, -cz + xy). \end{aligned}$$

Hence the system is dissipative when: $a < b + c$.

Science the system of Four-scroll attractor (3) is a dissipative system thus the solutions of the system of equations (3) are bounded as $t \rightarrow \infty$ for $a < b + c$. If $ab > 0, ac > 0$ and $bc > 0$ then the system has five equilibrium points:

$$\begin{aligned} E_0 &= (0, 0, 0), E_1 = (\sqrt{bc}, \sqrt{ac}, \sqrt{ab}), \\ E_2 &= (-\sqrt{bc}, -\sqrt{ac}, \sqrt{ab}), E_3 = (-\sqrt{bc}, \sqrt{ac}, -\sqrt{ab}), \\ E_4 &= (-\sqrt{bc}, -\sqrt{ac}, -\sqrt{ab}). \end{aligned}$$

Differing from other known similar systems, system (3) has five equilibrium, and does not have Hopf and pitch bifurcations [38, 39]. Of most interesting is the observation that this chaotic system not only can display a two-scroll chaotic attractor when $a=4.5, b=12$ and $c=5$ (Figure 1), but also can display a Four-scroll chaotic attractor when $a=0.4, b=12$ and $c=5$ (Figure 2).

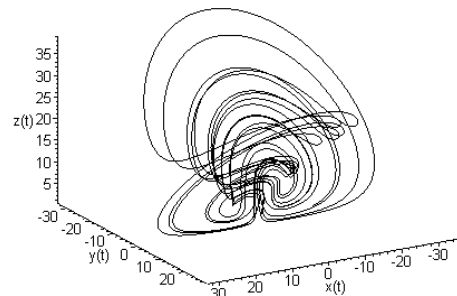


Figure 1: The chaotic attractor of two- scroll attractor at $a=4.5, b=12$ and $c=5$ in 3-dimensional.

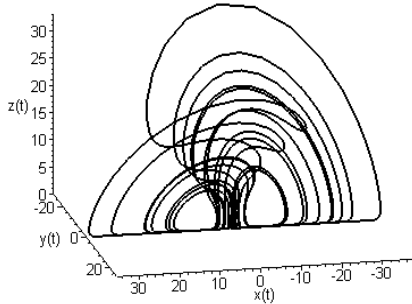


Figure 2: The chaotic attractor of Four- scroll attractor at $a=0.4$, $b=12$ and $c=5$ in 3-dimensional.

In this section we apply the generalized projective synchronization of two identical Four-scroll chaotic attractor. In order to observe the generalized projective synchronization behavior in the Four-scroll system, we have two Four-scroll systems where the drive system with three state variables denoted by the subscript 1 drives the response system having identical equations denoted by the subscript 2. However, the initial condition on the drive system is different from that of the response system. The two Four-scroll systems are described, respectively, by the following

$$\begin{aligned} \dot{x}_1 &= ax_1 - y_1 z_1 \\ \dot{y}_1 &= -by_1 + x_1 z_1 \\ \dot{z}_1 &= -cz_1 + x_1 y_1 \end{aligned} \tag{4}$$

and

$$\begin{aligned} \dot{x}_2 &= ax_2 - y_2 z_2 + u_1 \\ \dot{y}_2 &= -by_2 + x_2 z_2 + u_2 \\ \dot{z}_2 &= -cz_2 + x_2 y_2 + u_3 \end{aligned} \tag{5}$$

There are three control functions u_i , ($i=1, 2, 3$) to be determined later.

Define the error vector as

$e_x = x_2 - \alpha x_1$, $e_y = y_2 - \alpha y_1$ and $e_z = z_2 - \alpha z_1$ where α is a desired scaling factor. Then one obtains the error dynamical system by subtracting (4) from (5)

$$\begin{aligned} \frac{de_x}{dt} &= ae_x - y_2 z_2 + \alpha y_1 z_1 + u_1 \\ \frac{de_y}{dt} &= -be_y + x_2 z_2 - \alpha x_1 z_1 + u_2 \\ \frac{de_z}{dt} &= -ce_z + x_2 y_2 - \alpha x_1 y_1 + u_3 \end{aligned} \tag{6}$$

Referring to the original methods of active control, so we choose the three control functions u_i , ($i=1, 2, 3$) as follows:

$$\begin{aligned} u_1 &= y_2 z_2 - \alpha y_1 z_1 + v_1 \\ u_2 &= \alpha x_1 z_1 - x_2 z_2 + v_2 \end{aligned} \tag{7}$$

$$u_3 = \alpha x_1 y_1 - x_2 y_2 + v_3$$

then the error dynamical system (6) is described by

$$\begin{aligned} \frac{de_x}{dt} &= ae_x + v_1 \\ \frac{de_y}{dt} &= -be_y + v_2 \\ \frac{de_z}{dt} &= -ce_z + v_3 \end{aligned} \tag{8}$$

The error system (8) to be controlled is a linear system with a control input v_1 , v_2 and v_3 as function of the error e_x , e_y and e_z . As long as these feedbacks stabilize the system (8), e_x , e_y and e_z converge to zero as time tends to infinity, which implies that GPS of two identical Four-scroll systems is achieved with a scaling factor α . There are many possible choices for the control v_1 , v_2 and v_3 . In order to make the closed loop system (8) be stable, the proper choice of the control should guarantees that the feedback system must have all eigenvalues with negative real parts. For simplify, we choose

$$\begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} = A \begin{bmatrix} e_x \\ e_y \\ e_z \end{bmatrix} = \begin{bmatrix} -2a & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} e_x \\ e_y \\ e_z \end{bmatrix} \tag{9}$$

In this particular choice, the three eigenvalues of the closed loop system (8) are $-a$, $-b$ and $-c$. Since the closed loop system has all eigenvalues that are found to have negative real parts, the system will be convergence. In other words, this choice will result in a stable system and the GPS of two identical Four scroll systems. What deserves to be mentioned is that the values of the eigenvalues play an important role in the stability of the error system. In order to quicken the rate of convergence, we should make them get smaller.

2.1 Numerical Results

By using Maple 12, we select the parameters of the Four-scroll attractor as $a=0.4$, $b=12$ and $c=5$. The initial values of the drive system and response

system are taken as $x_1(0) = 0.23, y_1(0) = 0.1, z_1(0) = 0.32,$
 $x_2(0) = 1.77, y_2(0) = 0.9$ and $z_2(0) = 0.44$ respectively. If we take the scaling factor $\alpha = 2$ hence the error system has the initial values $e_x(0) = 1.29, e_y(0) = 0.7$ and $e_z(0) = -0.12$. then the generalized projective synchronization between two identical Four-scroll attractor are shown in Figure 3. If we take the scaling factor $\alpha = -0.2$ hence the error system has the initial values $e_x(0) = 1.818, e_y(0) = 0.94$ and $e_z(0) = -0.504$ then the GPS between two identical Four-scroll attractor are shown in Figure 4. If we take the scaling factor $\alpha = 1$ hence the error system has the initial values $e_x(0) = 1.54, e_y(0) = 0.8$ and $e_z(0) = 0.12$ then the complete synchronization between two identical Four-scroll attractor are shown in Figure 5. If we take the scaling factor $\alpha = -1$ hence the error system has the initial values $e_x(0) = 2, e_y(0) = 1$ and $e_z(0) = 0.76$ then the anti synchronization between two identical Four-scroll attractor are shown in Figure 6.

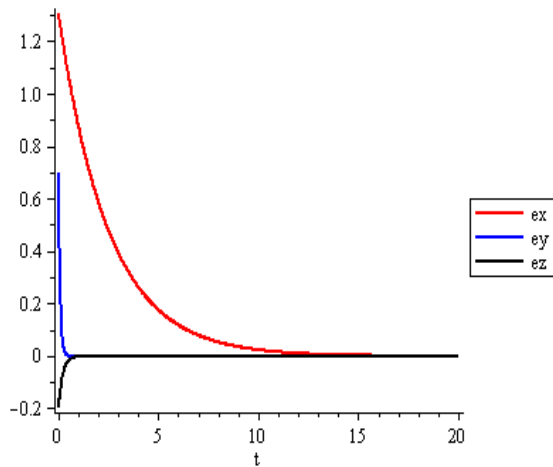


Figure 3: Shows the trajectories of e_x, e_y and e_z of two identical Four- scroll attractor with scaling factor $\alpha = 2$ for generalized projective synchronization.

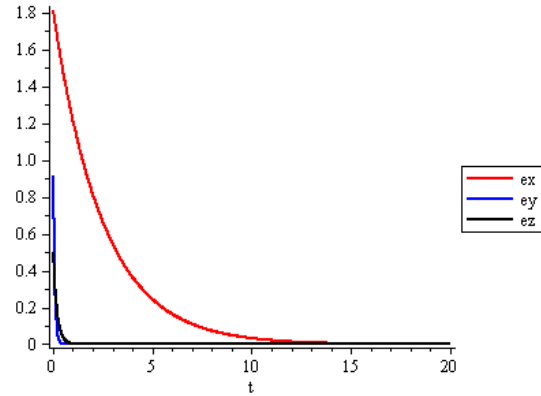


Figure 4 : The trajectories of e_x, e_y and e_z of two identical Four- scroll attractor with scaling factor $\alpha = -0.2$ for generalized projective synchronization.

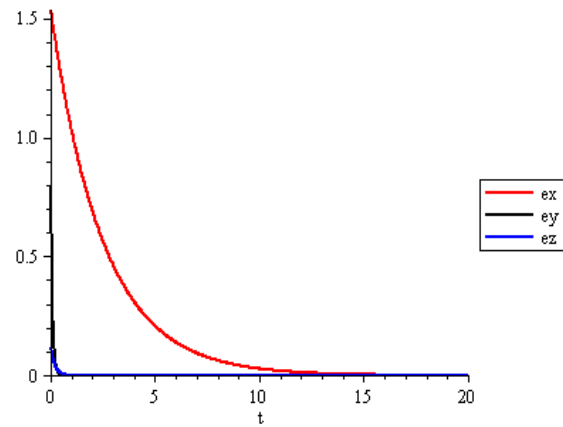


Figure 5: The trajectories of e_x, e_y and e_z of two identical Four- scroll attractor with scaling factor $\alpha = 1$ for complete synchronization.

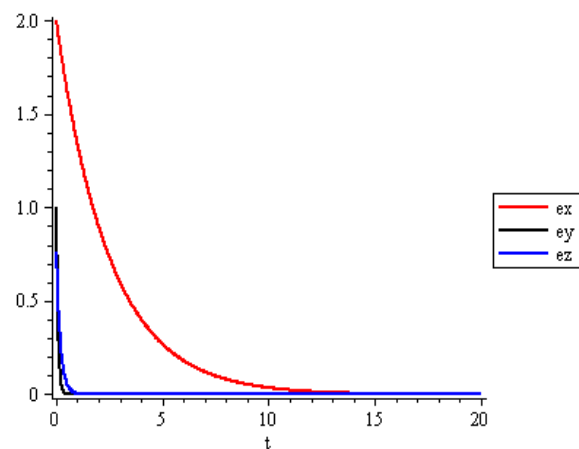


Figure 6: The trajectories of e_x, e_y and e_z of two identical four- scroll attractor with scaling factor $\alpha = -1$ for anti synchronization.

3. The application in secure communication

In this section, we will apply the adaptive scheme derived above to secure communication using the Four-scroll attractor. Assume that $m(t)$ is the message signal, adding it to the right hand side of the second equation for the transmitter (drive system), then we have

$$\begin{aligned} \dot{x}_1 &= ax_1 - y_1z_1 \\ \dot{y}_1 &= -by_1 + x_1z_1 + m(t) \\ \dot{z}_1 &= -cz_1 + x_1y_1 \end{aligned} \tag{9}$$

Select the output $y(t)$ of the system (9) as the transmitted signal, then construct the receiver as follows:

$$\begin{aligned} \dot{x}_2 &= ax_2 - y_2z_2 \\ \dot{y}_2 &= -by_2 + x_2z_2 + p(t) + u_1 \\ \dot{z}_2 &= -cz_2 + x_2y_2 + u_2 \\ \dot{p} &= -k(y_2 - \alpha y_1) \end{aligned} \tag{10}$$

where k is a positive parameter.

Let

$$e_1 = y_2 - \alpha y_1, e_2 = z_2 - \alpha z_1 \text{ and } e_3 = p - \alpha m$$

Then the error system can be described by

$$\begin{aligned} \dot{e}_1 &= -be_1 + x_1e_2 + e_3 + u_1 \\ \dot{e}_2 &= -ce_2 + x_1e_1 + u_2 \\ \dot{e}_3 &= -ke_1 - \alpha \frac{dm}{dt} \end{aligned} \tag{11}$$

Referring to the original methods of active control, so we choose the three control functions $u_i, (i = 1, 2)$ as follows:

$$u_1 = -x_1e_2 \text{ and } u_2 = -x_1e_1 \tag{12}$$

then the error dynamical system (11) is described by

$$\begin{aligned} \dot{e}_1 &= -be_1 + e_3 \\ \dot{e}_2 &= -ce_2 \\ \dot{e}_3 &= -ke_1 - \alpha \frac{dm}{dt} \end{aligned} \tag{13}$$

Then we take the Lyapunov function :

$$V(e) = \frac{1}{2}(ke_1^2 + e_2^2 + e_3^2) \tag{14}$$

It is clear that the Lyapunov function $V(e)$ is a positive definite function. Now, taking the time derivative of equation (14), then we get

$$\begin{aligned} \frac{dV(e)}{dt} &= ke_1\dot{e}_1 + e_2\dot{e}_2 + e_3\dot{e}_3 \\ &= -ke_1^2 + ke_1e_3 - ce_2^2 - ke_1e_3 - \alpha \frac{dm}{dt}e_1 \\ &= -ke_1^2 - ce_2^2 - \alpha \frac{dm}{dt}e_1 \end{aligned}$$

Since the eigen-frequency of the message signal $m(t)$ is much less than the oscillating frequency of the chaotic system in practice $\alpha \frac{dm}{dt} \approx 0$. It is easy

to have $\frac{dV(e)}{dt} < 0$. This can derive

$e_3 = p - \alpha m \rightarrow 0$ as $t \rightarrow \infty$, that is $\frac{p(t)}{\alpha}$ can recover the message signal $m(t)$.

Taking $m(t) = 0.1 \sin(0.1t), k = 100$, initial values

$$\begin{aligned} x_1(0) &= 0.23, y_1(0) = 0.1, z_1(0) = 0.32, \\ y_2(0) &= 0.9, z_2(0) = 0.4 \text{ and } p(0) = 6. \end{aligned}$$

Figures 7(a, b) show shows that the trajectory of e_3 of the error system with scaling factor $\alpha = 0.3$ and $\alpha = -0.4$, respectively.

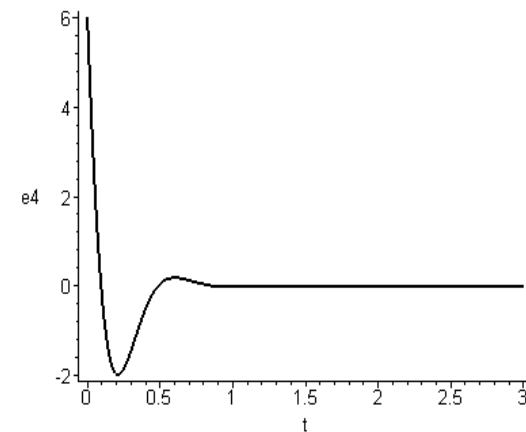


Fig. 7 (a): display the trajectory of e_3 of the error system with scaling factor $\alpha = 0.3$.

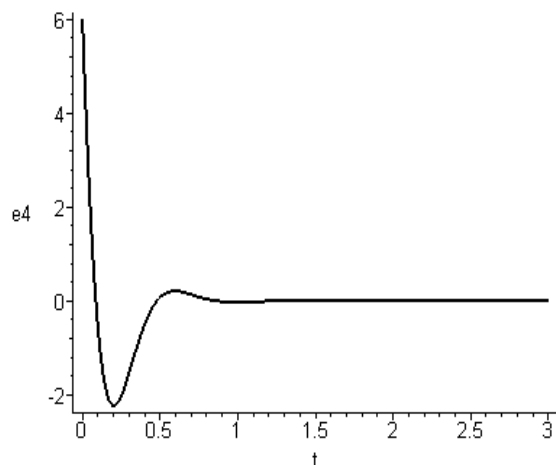


Fig. 7 (b): display the trajectory of e_3 of the error system with scaling factor $\alpha = -0.4$.

4. Conclusion

In this paper, an active control method is proposed for manipulating generalized projective synchronization in a general class of chaotic systems. This method is effective and convenient to generalized projective synchronize two identical systems and two different chaotic systems. Also we have proposed a scheme for a practical implementation of secure communication based on a active control method. Numerical simulations are also given to validate the proposed synchronization approach.

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